

A very compact CMOS class AB current mirror for Low Voltage Applications

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Abstract

This paper presents a compact bidirectional current mirror suitable for low voltage applications. The idea is to use complementary transistors in subthreshold which are able to set a reduced bias current through the mirror. The circuit presents a class AB operation with a THD near to 1% at 1MHz. The bandwidth is above 10MHz as shown by simulations using Spectre with 0.5 μ m CMOS technology parameters.

1. Introduction

The current mirror is a basic analog building block which is widely used in OTA's, OP-AMP's and other complex current mode circuits. Nowadays low-power requirements lead analog designers to consider class AB circuits due to their low quiescent current features and their capability to handle currents several times larger. Furthermore, voltage supply shrinking in modern fine line technology reduces considerably the voltage headroom for analog design; therefore, solutions capable to work with a low-voltage condition and class AB operation are mandatory. Many class AB current mirrors have been proposed. In [1], extra circuitry is included for achieving class AB operation but consequently, this extra complexity increases the minimum voltage requirement for the overall circuit. Other class AB approaches [2-4] improves the input/output impedance of the current mirror, however do not work for bidirectional currents and are not able to work for low-voltage applications. The low

impedance node of the FVF (*Flipped Voltage Follower*) has been extensively used for many applications including current mirrors [5-6]; in [5] the use of a FVF and a simple current mirror achieves class AB operation and low-voltage. Although an interesting solution, it is desirable to reach even simpler solutions at least for some applications. In this work, a very compact bidirectional current mirror is presented, which is able to deal with currents several orders of magnitude larger than the bias current.

This paper is organized as follows: In the next section the proposed circuit is presented and explained. Section 3 present simulations and discussion and finally; in section 4 some conclusions are given.

2. Compact class AB current mirror

The definition for a low-voltage circuit is given in [7]. A given circuit works in low-voltage mode if its voltage supply V_{DD} is less than the sum of the complementary threshold voltages of NMOS and PMOS, i.e. $V_{DD} < |V_{THp}| + V_{THn}$.

Figure 1, depicts the class AB current mirror proposed in [1]. Here transistors M3 and M4 set the bias current I_{bias} in the input branch. Therefore, these transistors can fix a reduced bias current for reduced static power consumption. Nevertheless, the branch of transistors M1 and M2 defines the minimum voltage supply requirement for the circuit, i.e. $V_{DDmin} = 2V_{DSsat} + V_{GSp} + V_{GSn}$. Where V_{DSsat} is the MOS overdrive drain-source voltage for saturation condition,

these considered from current sources I_{bias} implemented by a single transistor. V_{GSp} is the MOS voltage gate-source which must fulfill $V_{GSp} > |V_{THp}|$ and $V_{GSn} > V_{THn}$.

For $0.5\mu\text{m}$ CMOS technology with $V_{THn}=0.65\text{V}$ and $|V_{THp}|=0.95\text{V}$, this minimum supply must fulfill $V_{DDmin} > 2\text{V}$, so, the proposal is not suitable for low-voltage applications.

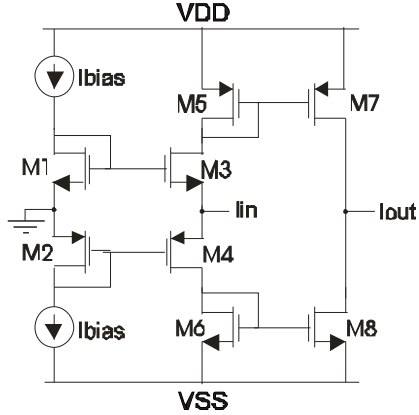


Figure 1.- Class AB current mirror

In Figure 2a) another class AB current mirror is presented [8], here the bias current at the input branch is defined by current sources I_{bias} . This input branch resembles that in Figure 1. Again the minimum supply required is $V_{DDmin} = 2V_{DSsat} + V_{GSp} + V_{GSn}$ which is not suitable for low voltage.

The proposed circuit is presented in figure 2b). This circuit is a simplified version of the two previous circuits.

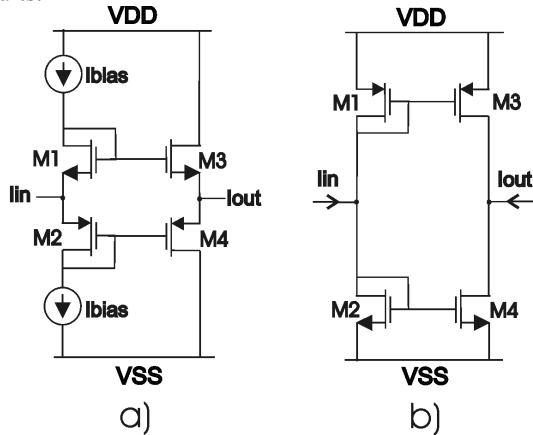


Figure 2.- a) Class AB current mirror, b) Proposed current mirror.

From Figure 1, the absence of transistors M3 and M4 lead to the circuit in Figure 2b). Since for low voltage operation $V_{DDmin} < |V_{THp}| + V_{THn}$, this condition leads M1 and M2 in Fig 2b) to work in subthreshold.

The MOS subthreshold conduction at drain has an exponential dependency on V_{GS} , for $V_{DS} > 200\text{mV}$ this is [9]:

$$I_D = I_0 \cdot \exp \frac{V_{GS}}{\zeta V_T} \quad (1)$$

Where $V_T = kT/q$, and $\zeta > 1$ is a nonideality factor.

This special feature fixes a very small bias current on both branches, preserving the class AB operation. Thus, when a given current i_{in} is introduced into the circuit the input node goes high turning M1 PMOS “off” and turning M2 NMOS “on”. Therefore, the input current is well copied by the M2-M4 mirror. In case i_{in} is extracted from the circuit, input node goes low, therefore, M2 NMOS is turned off and M1 turned on bringing i_{in} . In this case the input copy is achieved by the PMOS counterpart to the output.

3. Simulation Results

The circuit proposed in Figure 2b) was simulated using Spectre with BSIM3 ver 3.1 model parameters of ON Semi $0.5\mu\text{m}$ technology available through MOSIS. Transistors aspect ratio are $W/L=24.6\mu\text{m}/1.5\mu\text{m}$ for all NMOS and $W/L=73.8\mu\text{m}/1.5\mu\text{m}$ for PMOS transistors.

In Figure 3, the bias current of the circuit is plotted against different V_{DD} values. As can be noticed, bias current goes from several pA to μA .

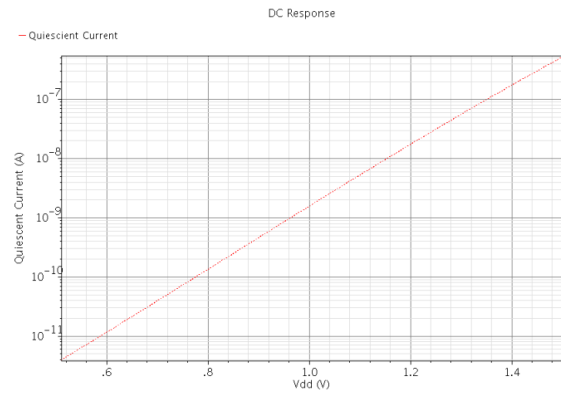


Figure 3.- DC simulations results, Bias current vs. V_{DD}

In Figure 4, a parametric DC sweep simulation of I_{in} vs I_{out} is shown, V_{DD} changes from 0.8V - 1.5V . The simulation shows the linearity of the current mirror for

different V_{DD} values. For $V_{DD} = 0.8V$, it is important to notice that the circuit handles more than 100,000 times its bias current, showing a class AB behavior.

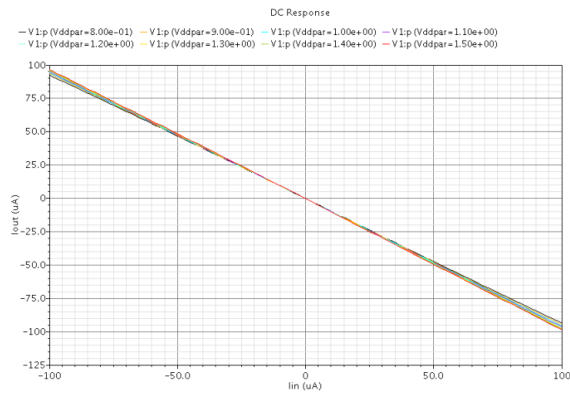


Figure 4.- Transfer function for different V_{DD} values.

Figure 5, shows the simulated AC response, the results show a cutoff frequency beyond 20MHz for $C_L=0$. Since the circuit only presents a high impedance node at the output it has an unconditionally stable behavior.

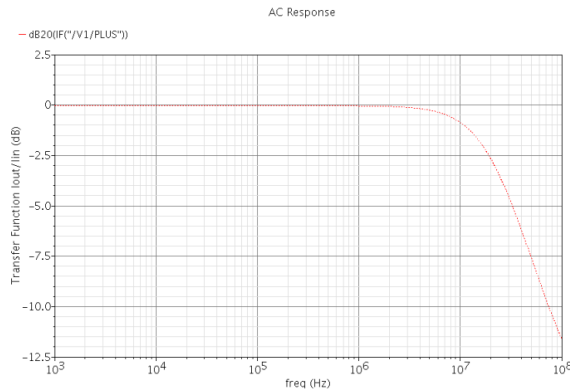


Figure 5.- AC simulation response.

The simulated output spectral response is shown in Figure 6, for $100\mu A_p @ 1MHz$ input signal. Distortion is introduced mainly by the third harmonic which is -49dB below the fundamental.

A Simulation of the input amplitude vs. THD is shown in Figure 7. As can be noticed maximum THD is 1.3% for $20\mu A_p$, 1MHz input signal.

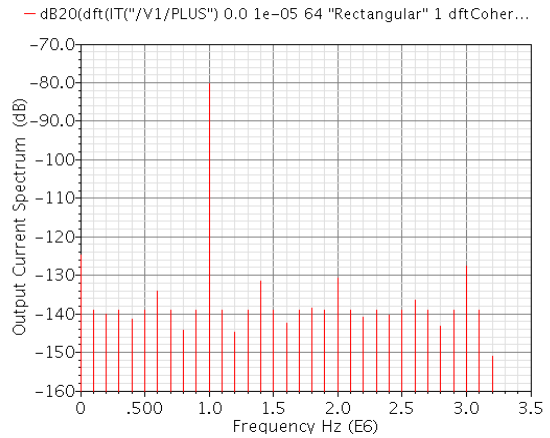


Figure 6.- Simulated output spectral response.

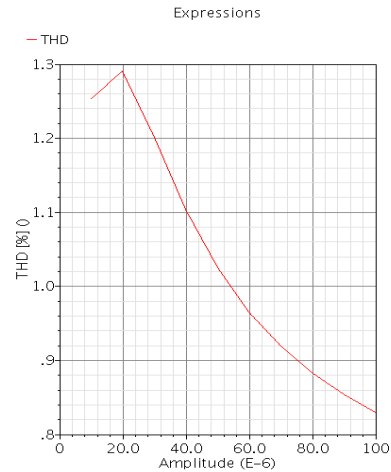


Figure 7.- Simulated input amplitude vs. THD.

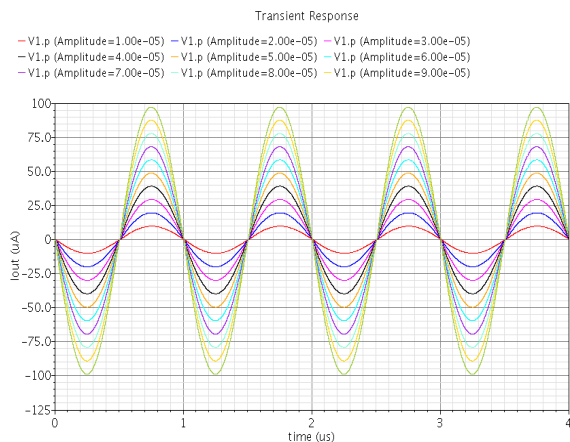


Figure 8.- Simulation of the current mirror transient response for several amplitudes

Finally, Figure 8, shows the current mirror transient response for several input amplitudes at 1MHz frequency.

4. Conclusions

In this work, a very compact low-voltage, class AB current mirror is presented. The circuit can drive currents at several orders of magnitude larger than its static current as shown through simulations. Since the circuit only presents a high impedance node, it has an unconditionally stable behavior and no compensating passive elements are required.

The simplicity of the circuit makes it feasible for many low-voltage applications.

5. References

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